WO 2004/096173

JC20 RECUPTIVIO 2 5 OU I ZUUS

Method for the dispersion of water-soluble or hydrophilic substances in a fluid at supercritical pressure

- 5 The present invention relates to a process for the dispersion of water-soluble or hydrophilic substances in a supercritical fluid.
- Many industrial processes, in particular in the pharmaceutical field, use dispersions of solid particles in an organic solvent or emulsions of an aqueous medium in an organic solvent. Mention will be made in particular of processes for encapsulation by coacervation of a coating agent dissolved in an organic solvent, bringing about the deposition of this coating agent at the surface of the particles suspended in the organic solution, and emulsion/solvent extraction or double emulsion processes.
- processes involve large amounts of organic 20 These such as halogenated solvents, and solvents, accompanied by high environmental costs. In pharmaceutical field, these processes require implementation of methods for monitoring the residual solvents and optionally for reducing the content of 25 residual solvent in pharmaceutical formulations. The trend is to reduce or even eliminate these solvents in processes intended for the production of pharmaceutical formulations. Finally, it is necessary to add that many pharmaceutical active principles, such as, for example, 30 therapeutic proteins, can be denatured by contact with an organic solvent.
- Carbon dioxide (CO<sub>2</sub>)at supercritical pressure finding increasing applications in numerous processes 35 where it advantageously substitutes for solvents. contrast to the dispersions in an organic solvent, the unique properties of CO2 at supercritical pressure make it possible, in the case of dispersions in  $CO_2$  at supercritical pressure, to separate the phases 40 simple decompression of the medium, thus resulting in easy recovery of the substances previously dispersed. These substances are furthermore devoid of residual organic solvent. The formation of dispersions in CO2 at supercritical pressure must thus offer advantageous 45 possibilities of substituting for organic solvents in major industrial processes, such as separations, reactions or processes for the formation of specific materials and in particular processes resulting pharmaceutical formulations in the form of powders. 50

The Applicant has endeavored to develop alternative processes free from organic solvent which make use of the advantageous properties of  $CO_2$  at supercritical The term "CO2 at supercritical pressure" pressure. denotes here CO2 brought to a pressure in the vicinity of or greater than its critical pressure (7.38 MPa). It can then be either in the liquid state or in the supercritical state. Thus, patent EP 0 784 506 B1 has as subject matter a process for the preparation of microparticles composed of solid particles which are insoluble in CO2 at supercritical pressure coated with a coating agent which is soluble in CO2 at supercritical The key stage of this process pressure. deposition of the coating agent on the particles in suspension in the supercritical fluid by controlled modification of the temperature and/or of the pressure of the supercritical fluid. The particles to be coated are conventionally dispersed in the supercritical fluid The improvements made to the abovestirring. 20 mentioned process have led the Applicant to look for means for improving the properties of dispersions of particles in the supercritical fluid, with the main stabilizing the dispersion and thus of object agglomeration of 25 reducing the phenomena of particles brought about by a difficulty in dispersing hydrophilic or water-soluble particles in a homogeneous supercritical stable manner in the fluid at and pressure.

30

10

15

Dispersions of solid particles are regarded as stable if, over time and under the effect of the various interactions which prevail in the dispersed system, the particles remain isolated and do not form reversible or the concentration 35 irreversible aggregates and particles remains homogeneous at every point in the dispersing medium, that is to say no phase separation appears. A loss in stability generally results first in the formation of aggregates of particles (flocculation, coagulation), related to the appearance of attractive 40 forces between the particles, and subsequently in a phase separation (sedimentation or creaming), due to the difference in density between the large aggregates dispersing medium (syneresis formed and the effect). The mechanisms for stabilizing dispersions of 45 solid particles are known to a person skilled in the and are described in the reference papers R.H. Ottewill (Journal of Colloid & Interface Science, No. 2, pp. 357-373, February 1977) and by Vol. 58, (Journal of Colloid æ Interface 50 J.Th.G. Overbeek Science, Vol. 58, No. 2, pp. 408-422, February 1977).

involve electrostatic interactions, when They particles carry electric charges at their surface which bring about repulsions between them and prevent the formation of aggregates. In the case of particles which do not carry electric charges, steric stabilization of 5 the dispersions can be obtained by introducing neutral (nonionic) polymer chains of well chosen length at the surface of the particles. These chains can either be attached chemically, on the one hand, or, on the other hand, can be adsorbed at the surface or physically 10 implanted in the surface layer of the dispersed solid particles. They must also exhibit a part which soluble in a good solvent in the dispersing phase. These chains thus exhibit a degree of surface-active or surfactant nature. The notion of steric stabilization 15 was initially introduced by W. Heller and T.L. Pugh in 1954 (Journal of Chemical Physics, Vol. 22, p. 1778, 1954). The stabilization is generated, on the one hand, by the repulsive forces related to the enthalpy of mixing of the stabilizing chains in a good solvent and, 20 on the other hand, by the elasticity of the polymer layer formed at the surface of the solid particles (entropic origin). The relative-contributions of these two mechanisms depend mainly on the temperature, on the good or poor solvating nature of the dispersing phase 25 and on the density and thickness of the stabilizing polymer. A complete review of steric layer of stabilization mechanisms is given in the reference paper by D.H. Napper (Journal of Colloid & Interface Science, Vol. 58, No. 2, pp. 390-407, 1977). An example 30 of the dispersion of hydrophobic (polyacrylonitrile) hydrophobic sterically stabilized in a particles (toluene) by polystyrene chains organic solvent adsorbed at their surface has been given by A. Doroszwski and R. Lambourne (Journal of Colloid & 35 Interface Science, Vol. 43, p. 97, 1973). Several examples of dispersions of solid hydrophilic (poly(12hydroxystearic acid), poly(oxyethylene)) particles in nonaqueous organic solvents (n-heptane, methanol) have 40 been given by D.H. Napper (Journal of Colloid Interface Science, Vol. 58, No. 2, pp. 390-407, 1977). Dense and hydrophilic inorganic particles of iron oxide have also been dispersed and sterically stabilized in cyclohexanone by polyamide chains adsorbed at their 45 (T. Sato, Journal of Coatings Technology, surface Vol. 65, No. 825, pp. 113-121, 1993).

The majority of commercial surfactants are insoluble in  $CO_2$  at supercritical pressure (Consani et al., Journal of Supercritical Fluids, 3 (1990), 51-65) and thus cannot be used to stabilize dispersions in  $CO_2$  at

50

supercritical pressure. However, a few surfactants soluble in CO2 at supercritical pressure are described in the literature. It is well known that the majority polymers are insoluble in CO2 at supercritical temperatures compatible with processes pressure at production of pharmaceutical intended for the formulations (Kirby C.F. and McHugh, Chemical Review, 565-602). A few families of CO<sub>2</sub>-philic (1999),polymers are substantially soluble in supercritical CO2. polymers are predominantly fluoropolymers 10 These (Newman D.A. et al., Journal of Supercritical Fluids, 6 305-210), such as poly(fluoroether)s, (1993),or poly(fluoromethacrylate)s, poly(fluoroacrylate)s silicones, such as poly (dimethylsiloxane)s (Hoefling et al., Journal of Supercritical Fluids, 6 (1993), 15 171) or poly(ether carbonate)s (Sarbu et al., Nature, 405 (2000), 165-167).

CO2-philic polymers have been employed to synthesize surfactants which can be used in  $CO_2$  at supercritical 20 They are either CO<sub>2</sub>-philic pressure. functionalized so as to increase their affinity for the substances to be dispersed or copolymers comprising chain members chosen from the polymers soluble in CO2 (CO<sub>2</sub>-soluble polymers) described previously. The main 25 applications of these surfactants are processes for polymerization in dispersion in supercritical CO2, where these surfactants make possible steric stabilization of the particles of polymers being formed. The chain members intended to interact with the particles of 30 polymers being formed are hydrophobic chain members, polystyrenes, as, for example, poly(vinyl acetate)s or poly(methyl methacrylate)s.

35 These compounds are all surfactants of the  $CO_2$ philic/hydrophobic type. They thus cannot be used to
stabilize dispersions of liquid or solid hydrophilic
substances in  $CO_2$  at supercritical pressure as they are
devoid of a hydrophilic part which can interact with
40 hydrophilic materials and become attached to their
surface.

CO2-philic surfactants with an ionizable head have been synthesized for the formation evaluated and 45 emulsions of water in supercritical CO2. These compounds composed of a CO<sub>2</sub>-philic part, such fluoropolymers or poly(siloxane)s, and of ionized head which can interact electrostatically with the aqueous phase to be dispersed. These surfactants 50 in some specific cases, made possible formation of emulsions or of microemulsions of water in supercritical CO2 (Hoefling T.A. et al., Journal of 95 (1991), 7127-7129). However, Physical Chemistry, they cannot be used to stabilize dispersions of solid hydrophilic particles in supercritical CO2, that is to say in a nonaqueous medium. This is because the stabilization of such dispersions requires a strong interaction of the surfactant with the surface of the dispersed, be making possible particles to permanent attachment of the polymer surfactants beyond the scope of their surface. Ιt is carrying a short ionizable polar head, surfactants which is furthermore nonionized in a nonaqueous medium.

5

10

45

50

inorganic Attempts at the steric stabilization of substances, such as particles of hydrophilic silica, 15 have been published (L. Calvo et al., Journal of 16 (2000), 247-260). Supercritical Fluids, this that the use of: demonstrated, in study, surfactants soluble in supercritical CO2, such as a perfluoropolyether carrying an ammonium carboxylate 20 short ionic head, or a polystyrene-poly(1,1-dihydroacrylate) copolymer, orperfluorooctyl poly(methyl methacrylate-co-hydroxyethyl methacrylate) copolymer grafted with polyfluoropolyether polymers, does not make possible the steric stabilization of 25 particles of hydrophilic silica with a size of greater in supercritical CO<sub>2</sub> starting from a than 1.2 µm dispersion of polydispersed particles (broad particle size distribution) of silica with a mean size of 3  $\mu m$ , 90% of which have a size of greater than 1.5  $\mu\text{m}.$  While 30 a suspension of the particles with a smaller diameter, of between 0.7 and 1.2 µm, is stabilized over a short period of time, only a minute fraction, less than 2.5%, of the mass of silica particles to be dispersed can be stabilized by these surfactants. These surfactants, 35 nevertheless soluble in supercritical CO2 and capable of stabilizing dispersions of hydrophobic substances supercritical CO2, thus do not make it possible to efficiently stabilize dispersions of particles of hydrophilic silica in supercritical CO2. 40

None of the  $CO_2$ -philic surfactants currently known thus makes it possible to prepare stable dispersions of water-soluble or hydrophilic solid substances in  $CO_2$  at supercritical pressure.

The inventors have found, surprisingly, that the use of block copolymers composed of at least one  $CO_2$ -philic block and of at least one nonionic hydrophilic block, of suitable composition and of suitable molar mass, makes it possible to prepare stable dispersions of

hydrophilic substances in CO2 at supercritical pressure.

The copolymers are chosen in particular from the group consisting of diblock copolymers and triblock copolymers, preferably diblock copolymers.

The triblock copolymers can correspond either to the formula (1)

10 hydrophilic/CO<sub>2</sub>-philic/hydrophilic (1),

or to the formula (2)

CO<sub>2</sub>-philic/hydrophilic/CO<sub>2</sub>-philic (2),

15

50

in which, respectively, the hydrophilic or  $\text{CO}_2\text{-philic}$  groups can be identical or different.

The present invention relates to the use of surfactants specifically designed to prepare stable dispersions of 20 water-soluble or hydrophilic substances in a fluid at supercritical pressure. These substances are in the liquid state under the temperature solid or pressure conditions of the process and are composed of 25 materials which are predominantly water-soluble or insoluble in CO<sub>2</sub> supercritical hydrophilic and at pressure.

The Applicant has designed and synthesized novel block copolymers comprising at least one CO2-philic block and 30 nonionic hydrophilic block. one copolymers have proved to be capable of stabilizing dispersions of hydrophilic solid particles in CO2 at supercritical pressure. They can be employed in particular for improving the encapsulation process 35 patent EP 0 784 506 B1. disclosed in copolymers are used both as agents for stabilizing the dispersion of hydrophilic particles and/or as coating copolymers can also be employed These surfactants for stabilizing a dispersion of particles 40 be coated, in conjunction with coating agents conventionally used in the abovementioned process, such as lipids, waxes, polymers or any compound which is sufficiently soluble in CO2 at supercritical pressure and which can be used in the implementation of the 45 abovementioned process.

It has been discovered, in the context of the present invention, that these specific surfactants can also be used for the formation and the steric stabilization of emulsions of water or of aqueous solutions in  $CO_2$  at

supercritical pressure.

35

40

The process which is a subject matter of the invention is particularly suitable for the production of pharmaceutical formulations, the processes for the preparation of which comprise a stage of dispersing water-soluble or hydrophilic substances in a dispersing medium composed of  $CO_2$  at supercritical pressure.

The dispersing medium is CO<sub>2</sub> brought to a pressure in the region of or greater than the critical pressure (7.38 MPa), preferably between 5 MPa and a pressure of 70 MPa, more preferably still between the critical pressure and a pressure of 30 MPa. The temperature is between 0°C and 100°C and preferably between 15°C and 60°C.

The dispersing medium can optionally comprise entrainer. Within the meaning of the present invention, an entrainer is defined as a substance deliberately 20 added in small amounts to the supercritical fluid so as to increase the solubility of one or more substance(s) in said supercritical fluid. When such an entrainer is present in a small amount in the supercritical fluid 25 (approximately < 5%), this amount is so low that it is essentially without effect on the conditions necessary for the entry into the supercritical state of the main supercritical fluid but the component of increases the solubility of the polymer material. Use may be made, as entrainer, by way of examples, 30 ketones, alcohols, esters and chlorinated solvents or plasticizers. other organic solvents and Such entrainers are particularly used when the polymer is not very soluble in CO2 at supercritical pressure.

In the case of dispersions of substances which are solid under the conditions of the process, the particles to be dispersed are composed of a hydrophilic or water-soluble material which is insoluble in the fluid at supercritical pressure, preferably particles comprising an active principle.

Water-soluble or hydrophilic substances or substances which are included in predominantly water-soluble or hydrophilic particles can be dispersed in CO<sub>2</sub> at supercritical pressure by the process which is a subject matter of the invention. Hydrophilic active principles or active principles dissolved or dispersed in a water-soluble or hydrophilic matrix are particularly employed in the formation of dispersions by the process of the invention.

Mention may nonexhaustively be made, among active pharmaceuticals, in particular of (i) principles, analgesics, antipyretics, aspirin and its derivatives, 5 antibiotics, anti-inflammatories, antiulceratives, antidepressants, neuroleptics, antihypertensives, oligonucleotides exhibiting a therapeutic activity, peptides exhibiting a therapeutic activity and proteins exhibiting a therapeutic activity, (ii) cosmetics, in particular self-tanning agents and UV stabilizers, and (iii) foodstuffs, such as, for example, vitamins.

10

The therapeutic proteins or peptides used in these formulations are preferably chosen from the protein corresponding to parathyroid hormone (PTH), growth 15 α-, βγ-interferons, αhormone (GH), or  $\beta$ -erythropoietin (EPO), granulocyte colony-stimulating granulocyte-macrophage colony-(GCSF), factor vasoactive intestinal stimulating factor (GMCSF), 20 (VIP), thyrotopin-releasing hormone (TRH), peptide angiotensin, insulin, vasopressin (AVP), arginine somatotropin, tissue plasminogen activator, clotting factors VIII and IX, glucosylceramidase, lenograstim, molgramostim, filgrastim, interleukins, dornase alfa, PEG-L-asparaginase, PEG-adenosine deaminase, hirudin, 25 factors, luteinizing eptacog alfa, nerve growth hormone-releasing hormone (LHRH), its derivatives and somatostatin derivatives, analogs, and its its gastrin-releasing triptorelin, bombesin, calcitonin, peptide, growth hormone-releasing factor and amylin. 30

The particles comprising an active principle which precipitation process for result from а crystallization using organic solvents or fluids at ' supercritical pressure, from a lyophilization process, 35 from a nebulization process, from a drying process or from a milling process which are capable of being dispersed in the fluid at supercritical pressure are preferably composed of a solid matrix comprising the active principle, in particular a therapeutic protein 40 or peptide, and optionally excipients, such as fillers, cryoprotectants stabilizers, protein lyoprotectants. Mention may nonexhaustively be made, among the excipients, of phosphate salts and other ionic compounds, sugars, polyols, filler proteins, such 45 as albumins, surfactants and any other substance used to stabilize solid formulations formed of therapeutic particles come. These existing or to proteins, comprising active principles, in particular proteins or peptides, are predominantly hydrophilic and difficult 50 to disperse in CO2 at supercritical pressure.

The size of the particles dispersed by the process which is a subject matter of the invention is between 0.05  $\mu m$  and 800  $\mu m$  and preferably between 0.1  $\mu m$  and 100  $\mu m$ .

The copolymers used in the process of the invention are block copolymers composed of a  $CO_2$ -philic block and of a nonionic hydrophilic block. The nature of the two blocks and their molar ratio can be altered and make possible fine adjustment of the properties for stabilization of dispersions of hydrophilic solids or liquids which are insoluble in  $CO_2$  at supercritical pressure.

15

10

5

The  $CO_2$ -philic block of the block copolymers is advantageously chosen from polymers which are soluble in  $CO_2$  at supercritical pressure.

The block copolymers are advantageously copolymers which are soluble in CO<sub>2</sub> at supercritical pressure. The minimum solubility of the block copolymers according to the invention is 0.05% w/w and preferably 0.2% w/w at at least one defined temperature which is between 0°C and 100°C, preferably at least one defined temperature which is between 15°C and 60°C, and at at least one defined pressure which is greater than the critical pressure of CO<sub>2</sub>, preferably less than 70 MPa and more preferably still less than 30 MPa.

30

35

40

The molar mass of the block copolymers which are subject matters of the invention and the molar ratio of the two  $CO_2$ -philic and hydrophilic blocks have to be chosen so as to give the copolymer a sufficient solubility in  $CO_2$  at supercritical pressure and a solubility which is advantageous for the process which is a subject matter of the invention, under temperature and pressure conditions which are technically and economically advantageous and which make possible the use of unstable substances, such as pharmaceutical active principles.

The molar mass and the molar ratio are also chosen in to the desired properties obtain With regard to these stabilization of dispersions. 45 considerations of solubility and of stabilization of the dispersions, it has been found, in the context of the present invention, that the number-average molar mass (Mn) of the copolymer has to be chosen between 50 1000 and 200 000 g/mol and more particularly between 4000 and 50 000 g/mol. The number-average molar mass of the hydrophilic block is between 500 and 20 000 g/mol and preferably between 1000 and 10 000 g/mol. The ratio by weight of the  $CO_2$ -philic block to the hydrophilic block, defined as the ratio of the number-average molar masses, is between 1 and 50 and preferably between 1 and 20.

Mention may in particular be made, among the polymers soluble in  ${\rm CO_2}$  used in the synthesis of the block poly(siloxane)s. and fluoropolymers of copolymers, 10polymers used fluoropolymers, the the Among poly(fluoroether)s, from chosen advantageously poly(fluoroalkyl methacrylate)s and poly(fluoroalkyl acrylate)s and particularly poly(1,1-dihydroperfluoropoly(1,1,2,2and PFOA acrylate)s or 15 octyl tetrahydroperfluorodecyl acrylate)s or PFDA.

The nonionic hydrophilic block is advantageously chosen from biocompatible hydrophilic polymers, in particular from the group consisting of polysaccharides, hydrophilic cellulose polymers, poly(vinyl alcohol), polyols, and ethylene oxide homo- and copolymers. Preferably, the hydrophilic block is a poly(ethylene oxide) or PEO.

20

25

30

35

40

The block copolymers used according to the process of the invention are advantageously block copolymers composed of a poly(1,1,2,2-tetrahydroperfluorodecyl acrylate) block and of a poly(ethylene oxide) block or are block copolymers of the PEO-b-PFDA type.

Mention may be made, among the triblock copolymers according to the invention, without implied limitation, of PFDA-b-PEO-b-PFDA triblock copolymers and PEO-b-PFDA-b-PEO triblock copolymers.

These copolymers are synthesized by any suitable synthetic route which offers access to the composition desired for the copolymer in terms of nature of the  $\text{CO}_2$ -philic and hydrophilic blocks, of molar mass and of molar ratio of the two blocks. The synthesis is preferably carried out by a conventional radical telomerization process.

The copolymers can be purified after synthesis by any 45 this purpose, such process commonly used for precipitations or chromatographic purifications, preferably by extraction or fractionation using  $CO_2$  at intrinsic their to due supercritical pressure uses extraction This medium. solubility in this 50 devices for continuous or batchwise conventional

extraction and fractionation by a supercritical fluid.

Hydrophilic substances are dispersed by any means commonly used to bring about the dispersion of solid or liquid substances in a fluid. In the case of dispersions of solid particles, the dispersing means preferred for the present invention are stirring by use of a rotating stirrer and fluidization by use of a bed fluidized with  $CO_2$  at supercritical pressure.

10

15

20

5

The use of these block copolymers is particularly beneficial in processes for coating or modifying substances dispersed in  $CO_2$  at supercritical pressure. This is because these processes can be improved by stabilization of the dispersion, limiting phenomena of aggregation.

The invention is thus of particular use in processes for the encapsulation of particles of pharmaceutical interest which are intended, for example, to improve the rheological behavior of powders, to improve the stability of the formulation, to modify their surface properties or to confer controlled release properties thereon.

25

30

35

The present invention is particularly suitable for processes for coating particles dispersed in CO2 at supercritical pressure, such as the process disclosed EP 0 784 506 B1, where а controlled patent modification of the temperature and/or of the pressure of CO<sub>2</sub> at supercritical pressure makes possible the controlled deposition of a coating agent which soluble in CO2 at supercritical pressure. The block copolymers are then used mainly as surfactants, making possible the stabilization of the dispersion, optionally as coating agents, alone or as a mixture with other coating agents.

The present invention also makes it possible to form and to stabilize emulsions of water or of aqueous solutions in CO<sub>2</sub> at supercritical pressure. Processes using a stage requiring the stabilization of emulsions of aqueous solutions in an organic solvent, such as, for example, the formation of hydrogels in inverse dispersion or emulsion, can advantageously benefit from the present invention, which makes it possible to replace organic solvents with carbon dioxide.

Another subject matter of the present invention is block copolymers composed of a CO<sub>2</sub>-philic block and of a biocompatible nonionic hydrophilic block.

The following examples and figures 1 to 6 and 8 to 10 illustrate the invention.

5 Examples 7 and 11 are comparative examples.

10

15

30

35

The appearance by scanning electron microscopy of the particles which have been subjected to an encapsulation process as described in example 1 is represented in figure 1.

A photograph of an emulsion of an aqueous solution of amaranth in supercritical  $CO_2$  at a temperature of  $40\,^{\circ}C$  and a pressure of 30 MPa, obtained in the presence of PEO-b-PFDA block copolymers according to the process of the invention, is represented in figure 2.

A photograph of a mixture of an aqueous solution of amaranth and of supercritical  $CO_2$  at a temperature of 40°C and a pressure of 30 MPa, with stirring but in the absence of PEO-b-PFDA block copolymer, is represented in figure 3.

A photograph of an emulsion of an aqueous solution of amaranth in liquid  $CO_2$  at a temperature of  $20\,^{\circ}C$  and a pressure of 30 MPa, obtained according to the process of the invention, is represented in figure 4.

### Example 1: Synthesis of a PEO-b-PFDA block copolymer

This example describes the synthesis of a block copolymer composed of a poly(ethylene oxide) block with a number-average molar mass (Mn) of 2000 g/mol (PEO 2000) and of a poly(1,1,2,2-tetrahydroperfluorodecyl acrylate) (PFDA) block, i.e. a diblock copolymer of the PEO-b-PFDA type. The synthesis is carried out by conventional radical telomerization.

In a first stage, a macromolecular telogen (I) is 40 synthesized from PEO 2000.

HO 
$$CH_2$$
-SH  $CH_3$ - $(OC_2H_4)n$ -OH  $CH_3$ - $(OC_2H_4)n$ -O  $CH_2$ -SH  $OC_2H_4$   $OC_2H_$ 

In a second stage, the telomerization of the fluoro-45 acrylate 1,1,2,2-tetrahydroperfluorodecyl acrylate (FDA) is carried out in the presence of the telogen (I) to form the block copolymer.

(I) 
$$\rightarrow$$
 O AIBN  $\rightarrow$  CH<sub>3</sub>—(OC<sub>2</sub>H<sub>4</sub>)<sub>e</sub>  $\rightarrow$  O  $\rightarrow$  CH<sub>2</sub>—S—(CH<sub>2</sub>—CH)<sub>e</sub>  $\rightarrow$  H  $\rightarrow$  O  $\rightarrow$  O  $\rightarrow$  O  $\rightarrow$  PEO-b-PFDA block copolymer  $\rightarrow$  C<sub>2</sub>H<sub>4</sub>C<sub>8</sub>F<sub>17</sub>

## 1.1. Synthesis of the macromolecular telogen (I)

50.03 g (25 mmol) of poly(ethylene oxide) monomethyl 5 ether (Aldrich,  $\overline{M}_n = 2000 \text{ g/mol}$ ) and 705.7 g of benzene are incorporated in a 1 liter three-necked equipped with a Dean and Stark apparatus, a reflux condenser and a magnetic flea. The polymer is dried by azeotropic entrainment at reflux (set temperature of 10 100°C) for 5 hours. Subsequently, 12.0243 q (127.9 mmol) of thioglycolic acid (Acros, 98%, M =92.11 g/mol) and 127 mg (0.658 mmol) of para-toluenesulfonic acid monohydrate (Aldrich, 98.5%) are added. The azeotropic entrainment is continued for 24 hours, 15 the water formed accumulated in the Dean and Stark apparatus being regularly withdrawn.

At the end of the reaction, the medium is brought back 20 to ambient temperature, filtered through a sintered glass No. 4, in order to remove a few insoluble materials, and then concentrated on a rotary evaporator at 40°C. 59.97 g of a viscous product are recovered, which product crystallizes at ambient temperature. It is dissolved in 31 g of chloroform (very viscous 25 This solution precipitated, solution). is 4 liters of ethyl ether cooled stirring, from beforehand in a freezer. Filtration is carried out through a sintered glass No. 4 and the cake is washed in the sintered glass with a further 1 liter of ethyl 30 ether at ambient temperature. 55.01 g of white powder are recovered, which powder is dried under vacuum  $(2 \times 10^{-2} \text{ mmHg})$  at 35-40°C for 2 hours. 45.87 g of white powder are finally obtained (yield = 88%).

## 1.2. Synthesis of a PEO-b-PFDA copolymer

35

The fluoroacrylate monomer 1,1,2,2-tetrahydroperfluorodecyl acrylate (FDA) is distilled under vacuum (P =  $3 \times 10^{-2}$  mmHq, 70-71°C). 40 The B.p. =azobisisobutyronitrile (AIBN) (Fluka, 98왕) recrystallized from methanol. The solvent, trifluoro-(TFT), is distilled under toluene (Lancaster, 99%) partial pressure (20 mmHg). The polymerization 45 carried out under argon in a two-necked 100 ml Schlenk reactor, closed with 2 turn-over closures,

magnetic stirring (magnetic flea).

fluoromonomer, placed in a sample tube, The deoxygenated by bubbling with argon (for 45 min). The 5 transfer agent and the initiator are placed in solution in the trifluorotoluene in the Schlenk reactor (slight heating with a heat gun to dissolve the telogen). The deoxygenated by bubbling with solution is (45 min). The monomer is added to the Schlenk reactor using a glass syringe while flushing with argon. The 10 Schlenk reactor is closed and is then placed in an oil bath at the desired temperature (65°C or 80°C). initial medium, cloudy after the addition of monomer, becomes clear with heating and with stirring after approximately 1 minute. Samples are withdrawn 15 through the septum with a glass syringe, the progress the reaction is monitored by <sup>1</sup>H NMR and the polymerization is halted by addition of hydroquinone. The final product is precipitated from ethyl ether (large excess), dried under vacuum at 30-35°C and then 20 stored in a cool place.

A first copolymer, referred to as P39, is synthesized with the following conditions:

25

FDA: w = 10.0522 g

TFT: w = 40.0 g (distilled)

AIBN: w = 4.9 mg

Telogen (I): w = 3.3194 g

 $30 T = 65^{\circ}C$ 

 $t_0+21h$  50: halting of the reaction

Due to its nonsolubility in conventional solvents, the copolymer cannot be analyzed unambiguously by steric exclusion chromatography. Analyses carried out by 1H NMR 35 (after dissolution in a TFT/Freon 113 mixture) and by elemental analysis make possible the determination of the molar ratio of the CO2-philic component (FDA) to the hydrophilic component (PEO). In view of the fact that the reaction product may comprise PEO homopolymers, 40 this ratio is the lower limit of the mean ratio of the CO<sub>2</sub>-philic components to the hydrophilic components of the block copolymer formed during the synthesis. The analyses show that the reaction product is composed copolymer 45 predominantly of а PEO-b-PFDA diblock composed of a PEO hydrophilic block with a numberaverage molar mass (Mn) of 2090 g/mol originating from the telogen (I) and of a PFDA CO2-philic block with a number-average molar mass of equal to or greater than 4869 g/mol. The ratio of the  $CO_2$ -philic and hydrophilic 50 blocks, calculated as the ratio of the molar mass Mn of

the PFDA  $CO_2$ -philic block to the molar mass Mn of the PEO hydrophilic block, is thus, for this polymer P39, equal to or greater than 2.4.

## Example 2: Synthesis of a series of PEO-b-PFDA block copolymers

10

15

20

25

30

35

40

A first series of PEO-b-PFDA block copolymers, referred to as P43, P44, P49, P50 and P52, based on the telogen (I) derived from PEO 2000, was synthesized so as to obtain a range of block copolymers with increasing CO2phile to hydrophile ratios by weight. The composition of the copolymer is adjusted by varying the weight of the FDA monomer and the weight of the telogen used in the synthesis. A second series of PEO-b-PFDA block conventional copolymers, obtained by radical telomerization from a telogen derived from a PEO with a molar mass Mn of 5000 g/mol by a synthetic route analogous to that described in example 1, was also synthesized. They are referred to as P45 and P48. The mean lower value of the CO<sub>2</sub>-phile to hydrophile ratio by weight of these copolymers, as described in example 1, is presented in table 1.

Table 1				
Copolymer	Lower limit of the PFDA/PEO ratio			
P43	6.4			
P44	7.2			
P49	37.8			
P50	28			
P52	18.9			
P45	1.2			
DAR	10.2			

Example 3: Determination of the solubility of the copolymers in  $CO_2$  at supercritical pressure

copolymers described of the The solubility examples 1 and 2 is evaluated using a device disclosed in detail in patent EP 0 784 506 Bl. This device is composed of a reactor with a maximum operating pressure of 30 MPa and with a volume of one liter equipped with a magnetically driven rotary stirring device. reactor is equipped with a water circulation jacket for regulating the temperature. A known weight of copolymer is introduced into a preweighed paper filter with a porosity of 2  $\mu m$ . The filter is then folded up and integrally attached to the upper part of the drive shaft of the stirring device, so as to provide mechanical confinement of the copolymer in this filter. The assembly is placed in the reactor. The stirring

rate is set at 460 revolutions per minute. Carbon dioxide is introduced into the reactor up to a pressure 20 MPa at a temperature of  $45\,^{\circ}\text{C}$ . The copolymer is pressure these temperature and extracted under 5 conditions for 1 hour. The temperature of the reactor approximately 23°C then reduced to approximately 30 minutes. The reactor is subsequently gradually brought to atmospheric pressure by opening a micrometric valve which allows the carbon dioxide to move towards a vent line at atmospheric pressure. After opening the reactor, the filter is recovered and weighed, so as to calculate the weight of the fraction dissolved in CO2 at supercritical pressure. The results the solubility measurements for the copolymers described in examples 1 and 2 are combined in table 2.

Table 2 Fraction dissolved at 45°C and 20 MPa

15

30

35

Copolymer	Sample (mg)	Fraction dissolved (%)	
P39	502.72	66.3	
P43	971.28	85.3	
P44	998.61	90.4	
P52	982.92	94.1	
P50	996.38	76	
P49	974.44	92.4	
P45	988.06	69.2	
P48	976.54	72.6	

20 This device for measuring the solubility in CO<sub>2</sub> at supercritical pressure is routinely used by Applicant. Due to the fact that, during the reduction in solvating power of the fluid, a portion of the dissolved coating agent is deposited on the surfaces of the filter, an extracted weight of the order of 90% is 25 commonly observed for compounds known as completely soluble in the fluid at supercritical pressure. The copolymers synthesized in examples 1 and 2 are thus soluble in CO2 at supercritical pressure.

#### Example 4: Cloud point curve of a copolymer

In order to quantify the solubility of the PEO-b-PFDA block copolymers in CO2 at supercritical pressure, the cloud point curve of the fraction extracted from the copolymer P44 as obtained in example 3 was drawn up using a variable-volume optical cell.

The cloud point pressures at various temperatures and at a constant fraction by weight of copolymer of 1.2% 40 with respect to the weight of CO<sub>2</sub> are presented in

table 3. At a pressure greater than the cloud point pressure, it is observed visually that the sample is completely soluble. At a pressure below the cloud point pressure, cloudiness is observed visually as a result of the precipitation of the copolymer. These results confirm the solubility of the copolymer in  $\text{CO}_2$  at supercritical pressure.

-		•	-		_
т	a	b		$^{\circ}$	-

10010 0				
Temperature (°C)	Pressure (MPa)			
65.2	23.23			
59.9	22.1			
55.2	20.6			
49.8	19.1			
45	17.6			
40.2	15.99			
35.3	14.3			
30.4	12.65			
25.7	10.74			
20.5	8.92			

## 10 Example 5: Dispersion of particles in supercritical CO<sub>2</sub>

#### 5.1. Procedure

The properties for stabilization of a dispersion of solid hydrophilic particles are evaluated indirectly in an encapsulation experiment as described in patent EP 0 784 506 B1.

The CO<sub>2</sub>-philic/hydrophilic block copolymer is thus used 20 here as dispersing agent and as coating agent. The experimental device is a device for encapsulation using supercritical CO<sub>2</sub> similar to that used in example 3, equipped with a reactor with an internal volume of 125 ml and with a maximum operating pressure of 30 MPa. The reactor is equipped with optical windows which make 25 it possible to observe the medium at supercritical pressure. 50 mg of spherical particles of ungrafted silica with a diameter of 50 µm (Nucleodur 100-50, Macherey-Nagel) are introduced into the reactor. 200 mg copolymer P39, described in example 1, are also 30 introduced. The reactor is equipped with a jacket which makes it possible to regulate its temperature. reactor is closed using a lid equipped with a stirring type. Stirring is anchor adjusted of dioxide 460 revolutions per minute. Carbon 35 introduced into the reactor until a pressure of 20 MPa a temperature of 45°C is obtained. Under these conditions, the copolymer is dissolved. A stable and silica particles dispersion of homogeneous 40 supercritical CO<sub>2</sub> is then observed.

After one hour, the temperature of the reactor is gradually reduced to 20°C over approximately 50 minutes, so as to bring about the deposition of the 5 copolymer at the surface of the particles. The pressure of the reactor is then reduced to atmospheric pressure over approximately 60 minutes, the carbon dioxide being allowed to escape in a controlled manner by opening a micrometric valve. After opening the reactor, the particles are recovered.

### 5.2. Results

10

35

The appearance of the particles recovered after having subjected to this encapsulation process 15 presented in figure 1.

The starting particles, which have remained separate, have been covered with a homogeneous layer of the copolymer over their entire surface, testifying to the 20 exposure of the whole of their surface to the coating agent. Furthermore, no agglomeration of the particles is recorded. During the use of hydrophobic coating example, triglycerides, agents, such as, for of agglomeration of the particles 25 phenomenon commonly observed by the Applicant with the same experimental conditions.

This result demonstrates the ability of the PEO-b-PFDA block copolymer P39 to stabilize a dispersion 30 hydrophilic particles in CO2 at supercritical pressure.

## Example 6: Formation of emulsions in the presence of supercritical CO2

#### 6.1. Procedure

The ability of the copolymers described in examples 1 and 2 to stabilize an emulsion is evaluated using a cell for observing phase equilibria at supercritical 40 pressure. This cell is composed of a cylinder made of stainless steel with a maximum operating pressure of 50 MPa and with a volume varying between 50 and 64 ml. The internal volume of the cell is adjusted via a actuated by pressurized nitrogen. 45 piston temperature of the medium is regulated by circulation silicone oil in a jacket. The medium can be homogenized using a magnetic bar rotated by magnetic stirring. The cylinder is equipped with two sapphire windows positioned facing one another. The cell is 50 illuminated via the rear window. The medium is observed

through the window situated at the front of the 22.5 ml of an aqueous cylinder. solution of a red hydrophilic dye, amaranth, are introduced into the high pressure cylinder. 200 mg of the copolymer P44 are also introduced into the cell. The cylinder is then closed using a lid equipped with a back-pressure piston. The volume is set at 50 ml via the piston. The temperature of the medium is maintained at 40°C. The cylinder is purged using a stream of carbon dioxide and then carbon 10 dioxide is introduced up to a pressure of 30 MPa while maintaining the volume at 50 ml. During introduction of the carbon dioxide, the white copolymer powder is gradually dissolved. The medium is then stirred and a red and opaque dispersed phase occupying 15 the entire volume of the cylinder is formed.

After 30 minutes, stirring is halted, and slow and gradual phase separation of the system is observed over approximately 5 minutes. A binary system is then observed and does not undergo change over a period of 2 hours. The lower part of the cell is red and opaque. The upper part is red and opalescent. It is an emulsion in  $CO_2$ , which are stable without stirring during the two hours of the experiment.

25

30

35

20

To confirm the role of the copolymer in the formation of this emulsion, the pressure is gradually reduced by gradually raising the piston. Destabilization of the emulsion then occurs and an upper phase becoming colorless and translucent and a lower phase comprising corresponding aggregates, to the copolymer undissolved because of the reduction in the solvating power of the supercritical dioxide, are observed. An in pressure makes increase it possible to dissolve the copolymer and to again form a water-in-CO2 emulsion.

#### 6.2. Results

40 A photograph of the medium seen from the front window of the reactor is represented in figure 2. The copolymer has thus made it possible to disperse, in the emulsion form, the aqueous dye solution in the supercritical carbon dioxide at a temperature of 40°C and a pressure of 30 MPa. An emulsion composed of droplets of the aqueous dye solution in CO<sub>2</sub> is formed.

# Example 7: Comparative example without use of block copolymers

## 7.1. Procedure

The experimental procedure described in example 6 is used but only the aqueous amaranth solution and the carbon dioxide are introduced into the cell

#### 10 7.2. Results

15

20

25

35

40

In the absence of copolymer and after stirring for one hour, two separate phases are observed in the cell with stirring (figure 3). The dense phase is translucent and red and the upper phase is translucent and colorless. Thus, there has been neither formation of emulsion nor of dissolution product of the hydrophilic dye in supercritical carbon dioxide at a temperature of 40°C and a pressure of 30 MPa.

An identical behavior is observed with a volume of aqueous amaranth solution of 7.5 ml and liquid carbon dioxide at a temperature of  $20\,^{\circ}\text{C}$  and a pressure of 20 MPa.

This comparative example confirms the role of the PEO-b-PFDA block copolymer in the formation of an emulsion of water in  $\rm CO_2$  at supercritical pressure.

## 30 Example 8: Formation of an emulsion in liquid CO<sub>2</sub> at supercritical pressure

A similar experiment to that of example 6 is carried out, except for the temperature, which is set at 20°C, and the volume of aqueous solution, set at 7.5 ml.

At this temperature and under the pressure conditions used, carbon dioxide at supercritical pressure is found in the liquid state. At  $20\,^{\circ}\text{C}$  and  $30\,\text{MPa}$ , an emulsion of water in liquid  $CO_2$  is formed after stirring, as presented in figure 4.

The PEO-b-PFDA block copolymer has thus made it possible to form an emulsion of an aqueous solution in liquid  $CO_2$  at supercritical pressure.

## Example 9: Dispersion of hydrophilic particles in supercritical CO<sub>2</sub>

50 The hydrophilic particles used in this example are particles comprising the excipients typically used for

formulating lyophilisates comprising therapeutic proteins. The hydrophilic particles are obtained by lyophilization of 100 ml of an aqueous solution comprising 8.39 g of glycine, 410 mg of human serum hydrogenphosphate albumin, 2.4 of sodium g dodecahydrate and 266 mg of sodium dihydrogenphosphate dihydrate. After lyophilization, the particles ground using an agate mortar and then sieved using a sieve with a mesh size of 25  $\mu m$ . The sieved particles with a size of less than 25 µm are recovered and used subsequently.

5

10

35

The ability of the copolymers described in examples 1 hydrophilic 2 to stabilize a dispersion of 15 particles is evaluated usina the cell for observation of phase equilibria described in example 6. 20 mg of hydrophilic particles and 200 mg of PEO-b-PFDA copolymer P44 described in example 2 are introduced into the high pressure cylinder of the observation cell. The temperature of the cylinder is adjusted to 20 45°C. The volume is set at 50 ml\_via\_the backpressure piston. The medium is stirred using a magnetic bar. Carbon dioxide is introduced into the cell until a pressure of 22 MPa is obtained. At this pressure, the 25 copolymer is dissolved and the particles are suspension in the medium. No particle is observed on the walls of the cylinder or on the sapphire windows. All the hydrophilic particles are therefore dispersed in the stirred medium in the presence of PEO-b-PFDA 30 block copolymer P44. Stirring is then halted. Slow the particles is observed. sedimentation of sedimentation time, determined by observation of the medium, is 10 minutes in the presence of the PEO-b-PFDA block copolymer P44.

Example 10: Dispersion of hydrophilic particles in liquid CO<sub>2</sub>.

An identical experiment is carried out at a temperature of  $25\,^{\circ}\text{C}$  and a pressure of  $11.5\,^{\circ}\text{MPa}$ . When the medium is stirred, all the particles of hydrophilic lyophilisate are dispersed in the liquid  $CO_2$  and no particles are observed on the walls. Stirring is then halted. Slow sedimentation of the particles is observed, with a sedimentation time of the order of 10 minutes.

Example 11: Comparative example without use of block copolymer

#### 11.1 In supercritical CO2

The experimental procedure described in example 9 is followed but only the hydrophilic particles are introduced into the cell before introduction of  $CO_2$ , without block copolymer P44.

cylinder high pressure is thermostatically controlled at 45°C. The pressure is increased up to 22 MPa by introduction of CO2. The medium is stirred via 10 a magnetic bar. It is observed that most of the particles are present on the internal walls of the high pressure cylinder and of the sapphire windows and are not dispersed in supercritical fluid. A few sporadic however, dispersed in 15 fine particles are, supercritical CO2. Rapid sedimentation of these sporadic dispersed particles is observed after stirring halted. The sedimentation time, determined by observing the sapphire window, medium through 20 approximately 90 seconds in this case.

### 11.2. In liquid CO<sub>2</sub>

Comparable results are obtained on attempting to disperse these particles in liquid CO<sub>2</sub> according to the procedure described in example 10, at a temperature of 25°C and at a pressure of 20 MPa. Most of the particles are observed on the walls of the cell and the sapphire windows. A few sporadic particles are dispersed in the liquid CO<sub>2</sub> if the medium is stirred. On halting the stirring, the sedimentation time is approximately 2 minutes.

#### 11.3. Conclusion

35

40

In the absence of block copolymers, the hydrophilic particles are therefore not effectively dispersed in supercritical or liquid  $CO_2$ . Vigorous stirring of the medium makes it possible to disperse only a small proportion of the particles in  $CO_2$  at supercritical pressure, most of the particles being found on the walls of the high pressure cylinder. Stopping the stirring brings about very rapid sedimentation of the sporadic hydrophilic particles dispersed by stirring.

45

50

These results, compared with those obtained in examples 9 and 10, confirm that, at 25°C or 45°C, thus for liquid or supercritical  $CO_2$ , the use of PEO-b-PFDA block copolymers makes it possible to efficiently disperse hydrophilic particles in  $CO_2$  at supercritical pressure.